Chapter 7, Solution 1.

(a) \( \tau = RC = 1/200 \)

For the resistor, \( V = iR = 56e^{-200t} = 8Re^{-200t} \times 10^{-3} \) \( \longrightarrow \) \( R = \frac{56}{8} = 7 \, \text{k}\Omega \)

\[ C = \frac{1}{200R} = \frac{1}{200 \times 7 \times 10^3} = 0.7143 \, \mu\text{F} \]

(b) \( \tau = 1/200 = 5 \, \text{ms} \)

(c) If value of the voltage at \( t = 0 \) is 56.

\[ \frac{1}{2} \times 56 = 56e^{-200t} \quad \longrightarrow \quad e^{200t} = 2 \]

\[ 200t_o = \ln 2 \quad \longrightarrow \quad t_o = \frac{1}{200} \ln 2 = 3.466 \, \text{ms} \]
Chapter 7, Solution 2.

\[ \tau = R_{th} C \]

where \( R_{th} \) is the Thevenin equivalent at the capacitor terminals.

\[ R_{th} = 120 \parallel 80 + 12 = 60 \, \Omega \]
\[ \tau = 60 \times 200 \times 10^{-3} = 12 \, s. \]
Chapter 7, Solution 3.

\[ R = 10 + \frac{20}{(20+30)} = 10 + \frac{40 \times 50}{(40+50)} = 32.22 \text{ k}\Omega \]

\[ \tau = RC = 32.22 \times 10^3 \times 100 \times 10^{-12} = 3.222 \mu\text{s} \]
Chapter 7, Solution 4.

For $t<0$, $v(0^-)=40$ V.

For $t>0$, we have a source-free RC circuit.

$\tau = RC = 2 \times 10^3 \times 10 \times 10^{-6} = 0.02$

$v(t) = v(0)e^{-t/\tau} = 40e^{-50t}$ V
Chapter 7, Solution 5.

Using Fig. 7.85, design a problem to help other students to better understand source-free RC circuits.

Although there are many ways to work this problem, this is an example based on the same kind of problem asked in the third edition.

Problem

For the circuit shown in Fig. 7.85, find $i(t)$, $t>0$.

![Figure 7.85 For Prob. 7.5.](image)

Solution

Let $v$ be the voltage across the capacitor.

For $t <0$,

$$v(0^-) = \frac{4}{2+4}(24) = 16 \text{ V}$$

For $t >0$, we have a source-free RC circuit as shown below.

$$\tau = RC = (4 + 5) \frac{1}{3} = 3 \text{ s}$$
v(t) = v(0)e^{-t/\tau} = 16e^{-t/3} V

i(t) = -C \frac{dv}{dt} = -\frac{1}{3} (-\frac{1}{3}) 16e^{-t/3} = 1.778e^{-t/3} A
Chapter 7, Solution 6.

\[ v_o = v(0) = \frac{2}{10 + 2} (40) = 6.667 \, V \]

\[ v(t) = v_o e^{-t/\tau}, \quad \tau = RC = 40 \times 10^{-6} \times 2 \times 10^3 = \frac{2}{25} \]

\[ v(t) = 6.667 e^{-12.5t} \, V \]
Chapter 7, Solution 7.

Assuming that the switch in Fig. 7.87 has been in position A for a long time and is moved to position B at t=0. Then at t = 1 second, the switch moves from B to C. Find $v_C(t)$ for $t \geq 0$.

Figure 7.87
For Prob. 7.7

Solution

Step 1. Determine the initial voltage on the capacitor. Clearly it charges to 12 volts when the switch is at position A because the circuit has reached steady state.

This then leaves us with two simple circuits, the first a 500 $\Omega$ resistor in series with a 2 mF capacitor and an initial charge on the capacitor of 12 volts. The second circuit which exists from $t = 1$ sec to infinity. The initial condition for the second circuit will be $v_C(1)$ from the first circuit. The time constant for the first circuit is $(500)(0.002) = 1$ sec and the time constant for the second circuit is $(1,000)(0.002) = 2$ sec. $v_C(\infty) = 0$ for both circuits.

Step 1.

$$v_C(t) = 12e^{-t} \text{ volts for } 0 < t < 1 \text{ sec and } 12e^{-1}e^{-2(t-1)} \text{ at } t = 1 \text{ sec, and}$$

$$= 4.415e^{-2(t-1)} \text{ volts for } 1 \text{ sec } < t < \infty.$$
Chapter 7, Solution 8.

(a) \[ \tau = RC = \frac{1}{4} \]
\[ -i = C \frac{dv}{dt} \]
\[ -0.2 e^{-4t} = C(10)(-4)e^{-4t} \quad \longrightarrow \quad C = 5 \text{ mF} \]
\[ R = \frac{1}{4C} = 50 \Omega \]

(b) \[ \tau = RC = \frac{1}{4} = 0.25 \text{ s} \]

(c) \[ w_c(0) = \frac{1}{2} CV_o^2 = \frac{1}{2} (5 \times 10^{-3})(100) = 250 \text{ mJ} \]

(d) \[ w_R = \frac{1}{2} \times \frac{1}{2} CV_o^2 = \frac{1}{2} CV_o^2 \left( 1 - e^{-2t_0/\tau} \right) \]
\[ 0.5 = 1 - e^{8t_0} \quad \longrightarrow \quad e^{8t_0} = \frac{1}{2} \]
or \[ e^{8t_0} = 2 \]
\[ t_0 = \frac{1}{8} \ln(2) = 86.6 \text{ ms} \]
Chapter 7, Solution 9.

For $t < 0$, the switch is closed so that

$$v_o(0) = \frac{4}{2+4} (6) = 4 \text{ V}$$

For $t > 0$, we have a source-free RC circuit.

$$\tau = RC = 3 \times 10^{-3} \times 4 \times 10^3 = 12 \text{ s}$$

$$v_o(t) = v_o(0) e^{-t/\tau} = 4e^{-t/12} \text{ V}.$$
Chapter 7, Solution 10.

For $t<0$, 

\[ v(0^-) = \frac{3}{3+9} (36V) = 9 \text{ V} \]

For $t>0$, we have a source-free RC circuit

\[ \tau = RC = 3\times10^3 \times 20 \times 10^{-6} = 0.06 \text{s} \]

\[ v_o(t) = 9e^{-16.667t} \text{ V} \]

Let the time be $t_o$.

\[ 3 = 9e^{-16.667t_o} \quad \text{or} \quad e^{16.667t_o} = \frac{9}{3} = 3 \]

\[ t_o = \frac{\ln(3)}{16.667} = 65.92 \text{ ms}. \]
Chapter 7, Solution 11.

For $t < 0$, we have the circuit shown below.

\[ \frac{4 || 4}{4 \times 4 / 8} = 2 \]

\[ i_o(0-) = \frac{2}{2 + 8} \times 6 = 1.2 \text{ A} \]

For $t > 0$, we have a source-free RL circuit.

\[ \tau = \frac{L}{R} = \frac{4}{4 + 8} = \frac{1}{3} \text{ thus,} \]

\[ i_o(t) = 1.2e^{-3t} \text{ A.} \]
Chapter 7, Solution 12.

Using Fig. 7.92, design a problem to help other students better understand source-free RL circuits.

Although there are many ways to work this problem, this is an example based on the same kind of problem asked in the third edition.

Problem

The switch in the circuit in Fig. 7.90 has been closed for a long time. At \( t = 0 \), the switch is opened. Calculate \( i(t) \) for \( t > 0 \).

![Figure 7.90](image)

Solution

When \( t < 0 \), the switch is closed and the inductor acts like a short circuit to dc. The 4 \( \Omega \) resistor is short-circuited so that the resulting circuit is as shown in Fig. (a).

\[
i(0^-) = \frac{12}{3} = 4 \text{ A}
\]

Since the current through an inductor cannot change abruptly,
\[
i(0) = i(0^-) = i(0^+) = 4 \text{ A}
\]
When \( t > 0 \), the voltage source is cut off and we have the RL circuit in Fig. (b).

\[
\tau = \frac{L}{R} = \frac{2}{4} = 0.5
\]

Hence,

\[
i(t) = i(0) e^{-t/\tau} = 4e^{-2} \, A
\]
Chapter 7, Solution 13.

(a) \( \tau = \frac{1}{10^3} = \frac{1\text{ms}}{10^3} = 1\text{ ms.} \)

\[ v(t) = i(t)R = 80e^{-1000t} \text{ V} = R5e^{-1000t} \times 10^{-3} \text{ or } R = \frac{80,000}{5} = 16\text{ k}\Omega. \]

But \( \tau = \frac{L}{R} = \frac{1}{10^3} \text{ or } L = \frac{16\times10^3}{10^3} = 16\text{ H.} \)

(b) The energy dissipated in the resistor is

\[ w = \int_0^\tau v(t)i(t)dt = \int_0^\tau 80e^{-1000t} \times 10^{-3} \times 5e^{-1000t} \times 10^{-3} \text{ d}t = \int_0^\tau \frac{400}{2000}e^{-2000t} \text{ d}t = \frac{0.4}{2000} - \frac{0.4}{2000}e^{-2000\tau} \]

\[ = 200(1-e^{-1}) \times 10^{-6} = 126.42 \mu\text{J.} \]

(a) 16 k\Omega, 16 H, 1 ms  \quad (b) 126.42 \mu\text{J}
Chapter 7, Solution 14.

\[ R_{th} = \frac{(40 + 20)}{(10 + 30)} = \frac{60 \times 40}{100} = 24 \Omega \]

\[ \tau = \frac{L}{R} = \frac{5 \times 10^{-3}}{24 \times 10^{3}} = 0.2083 \mu s \]
Chapter 7, Solution 15

(a) \( R_{Th} = 2 + 10//40 = 10\Omega \), \( \tau = \frac{L}{R_{Th}} = 5/10 = 0.5s \)

(b) \( R_{Th} = 40//160 + 48 = 40\Omega \), \( \tau = \frac{L}{R_{Th}} = (20\times10^{-3})/80 = 0.25\text{ ms} \)

(a) 10 \( \Omega \), 500 ms  (b) 40 \( \Omega \), 250 \( \mu \text{s} \)
Chapter 7, Solution 16.

\[ \tau = \frac{L_{eq}}{R_{eq}} \]

(a) \[ L_{eq} = L \quad \text{and} \quad R_{eq} = R_2 + \frac{R_1R_3}{R_1 + R_3} = \frac{R_2(R_1 + R_3) + R_1R_3}{R_1 + R_3} \]

\[ \tau = \frac{L(R_1 + R_3)}{R_2(R_1 + R_3) + R_1R_3} \]

(b) where \[ L_{eq} = \frac{L_1L_2}{L_1 + L_2} \quad \text{and} \quad R_{eq} = R_3 + \frac{R_2}{R_1 + R_2} = \frac{R_3(R_1 + R_2) + R_1R_2}{R_1 + R_2} \]

\[ \tau = \frac{L_1L_2(R_1 + R_2)}{(L_1 + L_2)(R_3(R_1 + R_2) + R_1R_2)} \]
Chapter 7, Solution 17.

\[ i(t) = i(0) e^{-\frac{t}{\tau}} \]

\[ \tau = \frac{L}{R_{eq}} = \frac{1/4}{4} = \frac{1}{16} \]

\[ i(t) = 6e^{-16t} \]

\[ v_o(t) = 3i + L \frac{di}{dt} = 18e^{-16t} + \frac{1}{4}(-16) 6e^{-16t} \]

\[ v_o(t) = -6e^{-16t}u(t) \text{ V} \]
Chapter 7, Solution 18.

If \( v(t) = 0 \), the circuit can be redrawn as shown below.

\[
\begin{align*}
\text{0.4 H} & \quad \text{\( R_{eq} \)} & \quad \text{\( v_o(t) \)} \\
\text{i(t)} & \quad \text{+} & \quad \text{–}
\end{align*}
\]

\[
R_{eq} = 2 \parallel 3 = \frac{6}{5}, \quad \tau = \frac{L}{R} = \frac{2}{5} \times \frac{6}{5} = \frac{1}{3}
\]

\[
i(t) = i(0)e^{t/\tau} = 5e^{-3t}
\]

\[
v_o(t) = -L \frac{di}{dt} = \frac{-2}{5}(-3)5e^{-3t} = 6e^{-3t} \text{ V}
\]
Chapter 7, Solution 19.

To find $R_{th}$ we replace the inductor by a 1-V voltage source as shown above.

$$10i_1 - 1 + 40i_2 = 0$$

But $i = i_2 + i/2$ and $i = i_1$

i.e. $i_1 = 2i_2 = i$

$$10i - 1 + 20i = 0 \quad \Rightarrow \quad i = \frac{1}{30}$$

$$R_{th} = \frac{1}{i} = 30 \Omega$$

$$\tau = \frac{L}{R_{th}} = \frac{6}{30} = 0.2 \text{ s}$$

$$i(t) = 6e^{-5t}u(t) \text{ A}$$
Chapter 7, Solution 20.

(a) \[ \tau = \frac{L}{R} = \frac{1}{50} \implies R = 50L \]
\[ v = -L \frac{di}{dt} \]
\[ 90e^{-50t} = -L(30)(-50)e^{-50t} \implies L = 60 \text{ mH} \]

(b) \[ \tau = \frac{L}{R} = \frac{1}{50} = 20 \text{ ms} \]

(c) \[ w = \frac{1}{2} Li^2(0) = \frac{1}{2}(0.06)(30)^2 = 27 \text{ J} \]

The value of the energy remaining at 10 ms is given by:
\[ w_{10} = 0.03(30e^{-0.5})^2 = 0.03(18.196)^2 = 9.933 \text{ J}. \]

So, the fraction of the energy dissipated in the first 10 ms is given by:
\[ \frac{27-9.933}{27} = 0.6321 \text{ or } 63.21\%. \]
Chapter 7, Solution 21.

The circuit can be replaced by its Thevenin equivalent shown below.

\[ V_{th} = \frac{80}{80 + 40} (60) = 40 \text{ V} \]

\[ R_{th} = 40 \parallel 80 + R = \frac{80}{3} + R \]

\[ I = i(0) = i(\infty) = \frac{V_{th}}{R_{th}} = \frac{40}{80/3 + R} \]

\[ w = \frac{1}{2} L I^2 = \frac{1}{2} (2) \left( \frac{40}{R + 80/3} \right)^2 = 1 \]

\[ \frac{40}{R + 80/3} = 1 \quad \rightarrow \quad R = \frac{40}{3} \]

\[ R = 13.333 \Omega \]
Chapter 7, Solution 22.

\[ i(t) = i(0) e^{-t/\tau}, \quad \tau = \frac{L}{R_{eq}} \]

\[ R_{eq} = 5 \parallel 20 + 1 = 5 \ \Omega, \quad \tau = \frac{2}{5} \]

\[ i(t) = 10e^{-2.5t} \ A \]

Using current division, the current through the 20 ohm resistor is

\[ i_o = \frac{5}{5 + 20} (-i) = \frac{-i}{5} = -2e^{-2.5t} \]

\[ v(t) = 20i_o = -40e^{-2.5t} \ V \]
Chapter 7, Solution 23.

Since the 2 $\Omega$ resistor, 1/3 H inductor, and the (3+1) $\Omega$ resistor are in parallel, they always have the same voltage.

\[-i = \frac{10}{2} + \frac{10}{3+1} = 7.5 \quad \rightarrow \quad i(0) = -7.5\]

The Thevenin resistance $R_{th}$ at the inductor’s terminals is

\[R_{th} = 2 \parallel (3+1) = \frac{4}{3}, \quad \tau = \frac{L}{R_{th}} = \frac{1/3}{4/3} = \frac{1}{4}\]

\[i(t) = i(0)e^{-t/\tau} = -7.5e^{-4t}, \quad t > 0\]

\[v_L = v_o = L\frac{di}{dt} = -7.5(-4)(1/3)e^{-4t}\]

\[v_o = 10e^{-4t} \text{ V}, \quad t > 0\]

\[v_x = \frac{1}{3+1}v_L = 2.5e^{-4t} \text{ V}, \quad t > 0\]
Chapter 7, Solution 24.

(a) \( v(t) = -5u(t) \)

(b) \( i(t) = -10[ u(t) - u(t - 3) ] + 10[ u(t - 3) - u(t - 5) ] \)
    \[ = -10u(t) + 20u(t - 3) - 10u(t - 5) \]

(c) \( x(t) = (t - 1)[ u(t - 1) - u(t - 2) ] + [ u(t - 2) - u(t - 3) ] \)
    \[ + (4 - t)[ u(t - 3) - u(t - 4) ] \]
    \[ = (t - 1)u(t - 1) - (t - 2)u(t - 2) - (t - 3)u(t - 3) + (t - 4)u(t - 4) \]
    \[ = r(t - 1) - r(t - 2) - r(t - 3) + r(t - 4) \]

(d) \( y(t) = 2u(-t) - 5[ u(t) - u(t - 1) ] \)
    \[ = 2u(-t) - 5u(t) + 5u(t - 1) \)
Chapter 7, Solution 25.

Design a problem to help other students to better understand singularity functions.

Although there are many ways to work this problem, this is an example based on the same kind of problem asked in the third edition.

Problem

Sketch each of the following waveforms.
(a) \( i(t) = [u(t-2)+u(t+2)] \) A
(b) \( v(t) = [r(t) - r(t-3) + 4u(t-5) - 8u(t-8)] \) V

Solution

The waveforms are sketched below.

(a) \( i(t) \) (A)

(b) \( v(t) \) (V)
Chapter 7, Solution 26.

(a) \( v_1(t) = u(t+1) - u(t) + \left[ u(t-1) - u(t) \right] \)
\( v_1(t) = u(t+1) - 2u(t) + u(t-1) \)

(b) \( v_2(t) = (4-t) \left[ u(t-2) - u(t-4) \right] \)
\( v_2(t) = -(t-4)u(t-2) + (t-4)u(t-4) \)
\( v_2(t) = 2u(t-2) - r(t-2) + r(t-4) \)

(c) \( v_3(t) = 2 \left[ u(t-2) - u(t-4) \right] + 4 \left[ u(t-4) - u(t-6) \right] \)
\( v_3(t) = 2u(t-2) + 2u(t-4) - 4u(t-6) \)

(d) \( v_4(t) = -t \left[ u(t-1) - u(t-2) \right] = -tu(t-1) + tu(t-2) \)
\( v_4(t) = (-t+1-1)u(t-1) + (t-2+2)u(t-2) \)
\( v_4(t) = -r(t-1) - u(t-1) + r(t-2) + 2u(t-2) \)
v(t) = [5u(t+1) + 10u(t) - 25u(t-1) + 15u(t-2)] V
Chapter 7, Solution 28.

\( i(t) \) is sketched below.
(c) \[ z(t) = \cos 4t \delta(t - 1) = \cos 4\delta(t - 1) = -0.6536\delta(t - 1) \], which is sketched below.
Chapter 7, Solution 30.

(a) \[ \int_{-\infty}^{\infty} 4t^2 \delta(t - 1) \, dt = 4t^2 \bigg|_{t=1} = 4 \]

(b) \[ \int_{-\infty}^{\infty} 4t^2 \cos(2\pi t) \delta(t - 0.5) \, dt = 4t^2 \cos(2\pi t) \bigg|_{t=0.5} = \cos \pi = -1 \]
Chapter 7, Solution 31.

(a) \[ \int_{-\infty}^{\infty} e^{-2t^2} \delta(t - 2) \, dt = e^{-4t^2} \bigg|_{t=2} = e^{-16} = 112 \times 10^{-9} \]

(b) \[ \int_{-\infty}^{\infty} [5 \delta(t) + e^{-t} \delta(t) + \cos 2\pi t \delta(t)] \, dt = \left( 5 + e^{-t} + \cos(2\pi t) \right) \bigg|_{t=0} = 5 + 1 + 1 = 7 \]
Chapter 7, Solution 32.

(a) \[ \int_{1}^{4} u(\lambda) d\lambda = \int_{1}^{4} 1 d\lambda = \lambda \bigg|_{1}^{4} = 4 - 1 = 3 \]

(b) \[ \int_{0}^{4} r(t - 1) dt = \int_{0}^{1} 0 dt + \int_{1}^{4} (t - 1) dt = \frac{t^2}{2} - t \bigg|_{1}^{4} = 4.5 \]

(c) \[ \int_{1}^{5} (t - 6)^2 \delta(t - 2) dt = (t - 6)^2 \bigg|_{t=2}^{16} = 16 \]
Chapter 7, Solution 33.

\[
i(t) = \frac{1}{L} \int_0^t v(t) \, dt + i(0)
\]

\[
i(t) = \frac{10^{-3}}{10 \times 10^{-3}} \int_0^t 15 \delta(t - 2) \, dt + 0
\]

\[
i(t) = 1.5 \, u(t - 2) \, A
\]
Chapter 7, Solution 34.

(a) \[
\frac{d}{dt} [u(t-1) u(t+1)] = \delta(t-1) u(t+1) + \\
u(t-1) \delta(t+1) = \delta(t-1)1 + 0 \delta(t+1) = \delta(t-1)
\]

(b) \[
\frac{d}{dt} [r(t-6) u(t-2)] = u(t-6) u(t-2) + \\
r(t-6) \delta(t-2) = u(t-6)1 + 0 \delta(t-2) = u(t-6)
\]

(c) \[
\frac{d}{dt} [\sin 4t u(t-3)] = 4 \cos 4t u(t-3) + \sin 4t \delta(t-3)
\]
\[
= 4 \cos 4t u(t-3) + \sin 4x3 \delta(t-3)
\]
\[
= 4 \cos 4t u(t-3) - 0.5366 \delta(t-3)
\]
Chapter 7, Solution 35.

(a) 
\[ v = Ae^{-2t}, \quad v(0) = A = -1 \]
\[ v(t) = -e^{-2t}u(t) \text{ V} \]

(b) 
\[ i = Ae^{3t/2}, \quad i(0) = A = 2 \]
\[ i(t) = 2e^{-1.5t}u(t) \text{ A} \]
Chapter 7, Solution 36.

(a) \( v(t) = A + Be^t, \quad t > 0 \)

\[
A = 1, \quad v(0) = 0 = 1 + B \quad \text{or} \quad B = -1
\]

\( v(t) = 1 - e^t \, V, \quad t > 0 \)

(b) \( v(t) = A + Be^{\sqrt{2}t}, \quad t > 0 \)

\[
A = -3, \quad v(0) = -6 = -3 + B \quad \text{or} \quad B = -3
\]

\( v(t) = -3(1 + e^{\sqrt{2}t}) \, V, \quad t > 0 \)
Chapter 7, Solution 37.

Let $v = v_h + v_p$, $v_p = 10$.

$$\dot{v}_h + \frac{1}{4} v_h = 0 \quad \longrightarrow \quad v_h = Ae^{-t/4}$$

$v = 10 + Ae^{-0.25t}$

$v(0) = 2 = 10 + A \quad \longrightarrow \quad A = -8$

$v = 10 - 8e^{-0.25t}$

(a) $\tau = 4s$

(b) $v(\infty) = 10$ V

(c) $v = \left(10 - 8e^{-0.25t}\right)u(t)$ V
Chapter 7, Solution 38.

Let \( i = i_p + i_h \)

\[ \dot{i}_h + 3i_h = 0 \quad \longrightarrow \quad i_h = A e^{-3t} u(t) \]

Let \( i_p = ku(t), \quad i_p = 0, \quad 3ku(t) = 2u(t) \quad \longrightarrow \quad k = \frac{2}{3} \)

\[ i_p = \frac{2}{3} u(t) \]

\[ i = (A e^{-3t} + \frac{2}{3}) u(t) \]

If \( i(0) = 0 \), then \( A + 2/3 = 0 \), i.e. \( A = -2/3 \). Thus,

\[ i = \frac{2}{3} (1 - e^{-3t}) u(t) \]
Chapter 7, Solution 39.

(a) Before $t = 0$,
\[ v(t) = \frac{1}{4+1}(20) = 4 \text{ V} \]

After $t = 0$,
\[ v(t) = v(\infty) + [v(0) - v(\infty)] e^{-t/\tau} \]
\[ \tau = RC = (4)(2) = 8, \quad v(0) = 4, \quad v(\infty) = 20 \]
\[ v(t) = 20 + (4 - 20)e^{-t/8} \]
\[ v(t) = 20 - 16e^{-t/8} \text{ V} \]

(b) Before $t = 0$, $v = v_1 + v_2$, where $v_1$ is due to the 12-V source and $v_2$ is due to the 2-A source.
\[ v_1 = 12 \text{ V} \]

To get $v_2$, transform the current source as shown in Fig. (a).
\[ v_2 = -8 \text{ V} \]

Thus,
\[ v = 12 - 8 = 4 \text{ V} \]

After $t = 0$, the circuit becomes that shown in Fig. (b).

\[ \begin{align*}
2 \text{ F} & \quad 4 \Omega \\
\underline{\text{+}} & \quad \underline{\text{\parallel}} & \quad \underline{\text{\parallel}} & \quad \underline{\text{\parallel}} & \quad \underline{\text{\parallel}} & \quad \underline{\text{\parallel}} & \quad \underline{\text{\parallel}} & \quad \underline{\text{\parallel}}
\end{align*} \]
\[ 8 \text{ V} \quad 12 \text{ V} \]

\[ \begin{align*}
\tau & = RC = (2)(3) = 6 \\
v(\infty) & = 12, \quad v(0) = 4, \quad v(t) = 12 + (4 - 12)e^{-t/6} \\
v(t) & = 12 - 8e^{-t/6} \text{ V}
\end{align*} \]
Chapter 7, Solution 40.

(a) Before \( t = 0 \), \( v = 12\, \text{V} \).
After \( t = 0 \),
\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]
\[ v(\infty) = 4, \quad v(0) = 12, \quad \tau = RC = (2)(3) = 6 \]
\[ v(t) = 4 + (12 - 4)e^{-t/6} \]
\[ v(t) = 4 + 8e^{-t/6} \, \text{V} \]

(b) Before \( t = 0 \), \( v = 12\, \text{V} \).
After \( t = 0 \),
\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]
After transforming the current source, the circuit is shown below.

![Circuit Diagram](attachment:4944870.png)

\[ v(0) = 12, \quad v(\infty) = 12, \quad \tau = RC = (2)(5) = 10 \]
\[ v = 12\, \text{V} \]
Chapter 7, Solution 41.

Using Fig. 7.108, design a problem to help other students to better understand the step response of an RC circuit.

Although there are many ways to work this problem, this is an example based on the same kind of problem asked in the third edition.

**Problem**

For the circuit in Fig. 7.108, find $v(t)$ for $t > 0$.

![Figure 7.108](image)

**Solution**

$v(0) = 0$, $v(\infty) = \frac{30}{36} (12) = 10$

$R_{cC} = (6 \parallel 30)(1) = \frac{(6)(30)}{36} = 5$

$v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau}$

$v(t) = 10 + (0 - 10) e^{-t/5}$

$v(t) = 10(1 - e^{-0.2t}) u(t)$
(a) \( v_o(t) = v_o(\infty) + \left[ v_o(0) - v_o(\infty) \right] e^{-t/\tau} \)

\[ v_o(0) = 0, \quad v_o(\infty) = \frac{4}{4+2} (12) = 8 \]

\[ \tau = R_{eq} C_{eq}, \quad R_{eq} = 2 \| 4 = \frac{4}{3} \]

\[ \tau = \frac{4}{3} (3) = 4 \]

\[ v_o(t) = 8 - 8e^{-t/4} \]

\[ v_o(t) = 8 \left(1 - e^{-0.25t}\right) \text{ V} \]

(b) For this case, \( v_o(\infty) = 0 \) so that

\[ v_o(t) = v_o(0) e^{-t/\tau} \]

\[ v_o(0) = \frac{4}{4+2} (12) = 8, \quad \tau = RC = (4)(3) = 12 \]

\[ v_o(t) = 8e^{-t/12} \text{ V} \]
Chapter 7, Solution 43.

Before \( t = 0 \), the circuit has reached steady state so that the capacitor acts like an open circuit. The circuit is equivalent to that shown in Fig. (a) after transforming the voltage source.

\[
0.5i \quad v_o
\]

\[
2 \text{ A}
\]

\[
40 \Omega
\]

\[
0.5i
\]

\[
80 \Omega
\]

(a)

\[
0.5i = 2 - \frac{v_o}{40}, \quad i = \frac{v_o}{80}
\]

Hence,

\[
\frac{1}{2} \frac{v_o}{80} = 2 - \frac{v_o}{40} \quad \Rightarrow \quad v_o = \frac{320}{5} = 64
\]

\[
i = \frac{v_o}{80} = 0.8 \text{ A}
\]

After \( t = 0 \), the circuit is as shown in Fig. (b).

\[
v_C(t) = v_C(0)e^{\frac{t}{\tau}}, \quad \tau = R_C C
\]

To find \( R_C \), we replace the capacitor with a 1-V voltage source as shown in Fig. (c).
\[ i = \frac{v_C}{80} = \frac{1}{80}, \quad i_o = 0.5i = \frac{0.5}{80} \]

\[ R_{th} = \frac{1}{i_o} = \frac{80}{0.5} = 160 \Omega, \quad \tau = R_{th}C = 480 \]

\[ v_C(0) = 64 \text{ V} \]

\[ v_C(t) = 64e^{-t/480} \]

\[ 0.5i = -i_C = -C \frac{dv_C}{dt} = -3 \left( \frac{1}{480} \right) 64e^{-t/480} \]

\[ i(t) = 800e^{-t/480} u(t) \text{ mA} \]
Chapter 7, Solution 44.

\[ R_{eq} = 6 \parallel 3 = 2 \Omega, \quad \tau = RC = 4 \]

\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]

Using voltage division,

\[ v(0) = \frac{3}{3+6} (60) = 20 V, \quad v(\infty) = \frac{3}{3+6} (24) = 8 V \]

Thus,

\[ v(t) = 8 + (20 - 8) e^{-t/4} = 8 + 12 e^{-t/4} \]

\[ i(t) = C \frac{dv}{dt} = (2)(12) \left( \frac{-1}{4} \right) e^{-t/4} = -6 e^{-0.25t} \ A \]
Chapter 7, Solution 45.

To find $R_{Th}$, consider the circuit shown below.

\[ R_{th} = 10 + \frac{20}{40} = 10 + \frac{20 \times 40}{60} = \frac{70}{3} \, \text{k}\Omega \]

\[ \tau = R_{th}C = \frac{70}{3} \times 10^3 \times 3 \times 10^{-6} = 0.07 \]

To find $v_o(\infty)$, consider the circuit below.

\[ v_o(\infty) = \left[ \frac{40}{40+20} \right] 30 = 20 \, \text{V} \]

\[ v_o(t) = v_o(\infty) + [v_o(0) - v_o(\infty)]e^{-t/\tau} = [20 - 15e^{-14.286t}]u(t) \, \text{V}. \]
Chapter 7, Solution 46.

\[ \tau = R_{in} C = (2 + 6) \times 0.25 = 2 \text{s}, \quad v(0) = 0, \quad v(\infty) = 6i_0 = 6 \times 5 = 30 \]

\[ v(t) = v(\infty) + [v(0) - v(\infty)]e^{-t/\tau} = 30(1 - e^{-t/\tau}) u(t) \text{ V} \]
Chapter 7, Solution 47.

For $t < 0$, $u(t) = 0$, \quad u(t - 1) = 0, \quad v(0) = 0$

For $0 < t < 1$, \quad $\tau = RC = (2 + 8)(0.1) = 1$
\begin{align*}
  v(0) &= 0, \quad v(\infty) = (8)(3) = 24 \\
  v(t) &= v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \\
  v(t) &= 24\left(1 - e^{-t}\right)
\end{align*}

For $t > 1$, \quad $v(1) = 24\left(1 - e^{-1}\right) = 15.17$
\begin{align*}
  -6 + v(\infty) - 24 &= 0 \quad \rightarrow \quad v(\infty) = 30 \\
  v(t) &= 30 + (15.17 - 30)e^{-t(1)} \\
  v(t) &= 30 - 14.83e^{-t(1)}
\end{align*}

Thus,
\[
v(t) = \begin{cases} 
  24\left(1 - e^{-t}\right) V, & 0 < t < 1 \\
  30 - 14.83e^{-t(1)} V, & t > 1
\end{cases}
\]
Chapter 7, Solution 48.

For $t < 0$, \[ u(-t) = 1 \, , \]

For $t > 0$, \[ u(-t) = 0, \quad v(\infty) = 0 \]

\[ R_{th} = 20 + 10 = 30, \quad \tau = R_{th} C = (30)(0.1) = 3 \]

\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]

\[ v(t) = 10 e^{-t/3} \, V \]

\[ i(t) = C \frac{dv}{dt} = (0.1) \left( \frac{-1}{3} \right) 10 e^{-t/3} \]

\[ i(t) = \frac{-1}{3} e^{-t/3} \, A \]
Chapter 7, Solution 49.

For $0 < t < 1$, $v(0) = 0$, $v(\infty) = (2)(4) = 8$

$R_{eq} = 4 + 6 = 10$, $\tau = R_{eq}C = (10)(0.5) = 5$

$v(t) = v(\infty) + [v(0) - v(\infty)] e^{-t/\tau}$

$v(t) = 8\left(1 - e^{-t/5}\right) \ V$

For $t > 1$,

$v(1) = 8\left(1 - e^{-0.2}\right) = 1.45$, $v(\infty) = 0$

$v(t) = v(\infty) + [v(1) - v(\infty)] e^{-(t-1)/\tau}$

$v(t) = 1.45 e^{-(t-1)/5} \ V$

Thus,

$v(t) = \begin{cases} 
8\left(1 - e^{-t/5}\right) \ V, & 0 < t < 1 \\
1.45 e^{-(t-1)/5} \ V, & t > 1 
\end{cases}$
Chapter 7, Solution 50.

For the capacitor voltage,
\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]
\[ v(0) = 0 \]

For \( t > 0 \), we transform the current source to a voltage source as shown in Fig. (a).

We now obtain \( i_x \) from \( v(t) \). Consider Fig. (b).

\[ i_x = 30 \text{ mA} - i_T \]

But
\[ i_T = \frac{v}{R_3} + C \frac{dv}{dt} \]
\[ i_T(t) = 7.5(1 - e^{-4t}) \text{ mA} + \frac{1}{4} \times 10^{-3} (-15)(-4)e^{-4t} \text{ A} \]
\[ i_T(t) = 7.5(1 + e^{-4t}) \text{ mA} \]

Thus,
\[ i_x(t) = 30 - 7.5 - 7.5 e^{-4t} \text{ mA} \]
\[ i_x(t) = 7.5(3 - e^{-4t}) \text{ mA}, \quad t > 0 \]
Consider the circuit below.

After the switch is closed, applying KVL gives

\[ V_S = R i + L \frac{di}{dt} \]

or

\[ L \frac{di}{dt} = -R \left( i - \frac{V_S}{R} \right) \]

\[ \frac{di}{i - V_S/R} = -\frac{R}{L} dt \]

Integrating both sides,

\[ \ln \left( i - \frac{V_S}{R} \right) \bigg|_0^t = -\frac{R}{L} t \]

\[ \ln \left( \frac{i - V_S/R}{I_0 - V_S/R} \right) = -\frac{t}{\tau} \]

or

\[ \frac{i - V_S/R}{I_0 - V_S/R} = e^{-t/\tau} \]

\[ i(t) = \frac{V_S}{R} + \left( I_0 - \frac{V_S}{R} \right) e^{-t/\tau} \]

which is the same as Eq. (7.60).
Chapter 7, Solution 52.

Using Fig. 7.118, design a problem to help other students to better understand the step response of an RL circuit.

Although there are many ways to work this problem, this is an example based on the same kind of problem asked in the third edition.

Problem

For the circuit in Fig. 7.118, find \( i(t) \) for \( t > 0 \).

![Figure 7.118](image)

Solution

\[
\begin{align*}
i(0) &= \frac{20}{10} = 2 \text{ A}, \quad i(\infty) = 2 \text{ A} \\
i(t) &= i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau} \\
i(t) &= 2 \text{ A}
\end{align*}
\]
Chapter 7, Solution 53.

(a) Before $t = 0$, \[ i = \frac{25}{3+2} = 5 \text{ A} \]

After $t = 0$, \[ i(t) = i(0)e^{-t/\tau} \]

\[ \tau = \frac{L}{R} = \frac{4}{2} = 2, \quad i(0) = 5 \]

\[ i(t) = 5e^{-t/2} u(t) \text{ A} \]

(b) Before $t = 0$, the inductor acts as a short circuit so that the $2 \Omega$ and $4 \Omega$ resistors are short-circuited.

\[ i(t) = 6 \text{ A} \]

After $t = 0$, we have an RL circuit.

\[ i(t) = i(0)e^{-t/\tau}, \quad \tau = \frac{L}{R} = \frac{3}{2} \]

\[ i(t) = 6e^{-2t/3} u(t) \text{ A} \]
Chapter 7, Solution 54.

(a) Before $t = 0$, $i$ is obtained by current division or

$$i(t) = \frac{4}{4+4} (2) = 1 \text{ A}$$

After $t = 0$,

$$i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau}$$

$$\tau = \frac{L}{R_{eq}}, \quad R_{eq} = 4 + (4 \parallel 12) = 7 \Omega$$

$$\tau = \frac{3.5}{7} = \frac{1}{2}$$

$$i(0) = 1, \quad i(\infty) = \frac{(4 \parallel 12)}{4 + (4 \parallel 12)} (2) = \frac{3}{4} (2) = \frac{6}{7}$$

$$i(t) = \frac{6}{7} + \left( 1 - \frac{6}{7} \right) e^{-2t}$$

$$i(t) = \frac{1}{7} \left( 6 - e^{-2t} \right) \text{ A}$$

(b) Before $t = 0$, \( i(t) = \frac{10}{2+3} = 2 \text{ A} \)

After $t = 0$, \( R_{eq} = 3 + (6 \parallel 2) = 4.5 \)

$$\tau = \frac{L}{R_{eq}} = \frac{2}{4.5} = \frac{4}{9}$$

$$i(0) = 2$$

To find $i(\infty)$, consider the circuit below, at $t = \ldots$ when the inductor becomes a short circuit,

\[
\begin{align*}
10 \text{ V} & \quad 24 \text{ V} \\
2 \Omega & \quad 6 \Omega & \quad 3 \Omega \\
\end{align*}
\]

\[
\begin{align*}
\frac{10 - v}{2} + \frac{24 - v}{6} &= \frac{v}{3} \\
i(t) &= 3 + (2 - 3)e^{-9t/4} \\
\end{align*}
\]

$$v = 9 \quad i(\infty) = \frac{v}{3} = 3 \text{ A \ and}$$

$$i(t) = 3 - e^{-9t/4} \text{ A}$$
Chapter 7, Solution 55.

For $t < 0$, consider the circuit shown in Fig. (a).

\[
3i_o + 24 - 4i_o = 0 \quad \Rightarrow \quad i_o = 24
\]

\[
v(t) = 4i_o = 96 \text{ V} \quad \quad i = \frac{v}{2} = 48 \text{ A}
\]

For $t > 0$, consider the circuit in Fig. (b).

\[
i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau}
\]

\[
i(0) = 48, \quad i(\infty) = 0
\]

\[
R_{th} = 2 \Omega, \quad \tau = \frac{L}{R_{th}} = \frac{0.5}{2} = \frac{1}{4}
\]

\[
i(t) = (48)e^{-4t}
\]

\[
v(t) = 2i(t) = 96e^{-4t} u(t)V
\]
Chapter 7, Solution 56.

\[ R_{eq} = 6 + 20 \parallel 5 = 10 \, \Omega, \quad \tau = \frac{L}{R} = 0.05 \]

\[ i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau} \]

\[ i(0) \text{ is found by applying nodal analysis to the following circuit.} \]

\[ \begin{align*}
2 + \frac{20 - v_x}{5} &= \frac{v_x}{12} + \frac{v_x}{20} + \frac{v_x}{6} \\
v_x &= 12 \\
i(0) &= \frac{v_x}{6} = 2 \, \text{A}
\end{align*} \]

Since \( 20 \parallel 5 = 4 \),

\[ i(\infty) = \frac{4}{4 + 6} \cdot (4) = 1.6 \]

\[ i(t) = 1.6 + (2 - 1.6)e^{-t/0.05} = 1.6 + 0.4e^{-20t} \]

\[ v(t) = L \frac{di}{dt} = \frac{1}{2} (0.4)(-20)e^{-20t} \]

\[ v(t) = -4e^{-20t} \, \text{V} \]
Chapter 7, Solution 57.

At $t = 0^-$, the circuit has reached steady state so that the inductors act like short circuits.

\[
i = \frac{30}{6 + (5 \parallel 20)} = \frac{30}{10} = 3, \quad i_1 = \frac{20}{25} (3) = 2.4, \quad i_2 = 0.6
\]

$i_1(0) = 2.4 \text{ A}, \quad i_2(0) = 0.6 \text{ A}$

For $t > 0$, the switch is closed so that the energies in $L_1$ and $L_2$ flow through the closed switch and become dissipated in the 5 $\Omega$ and 20 $\Omega$ resistors.

\[
i_1(t) = i_1(0) e^{-t/\tau_1}, \quad \tau_1 = \frac{L_1}{R_1} = \frac{2.5}{5} = \frac{1}{2}
\]

\[
i_1(t) = 2.4e^{-2t}u(t) \text{ A}
\]

\[
i_2(t) = i_2(0) e^{-t/\tau_2}, \quad \tau_2 = \frac{L_2}{R_2} = \frac{4}{20} = \frac{1}{5}
\]

\[
i_2(t) = 600e^{-5t}u(t) \text{ mA}
\]
Chapter 7, Solution 58.

For \( t < 0 \), \( v_o(t) = 0 \)

For \( t > 0 \), \( i(0) = 10 \), \( i(\infty) = \frac{20}{1+3} = 5 \)

\[
R_{th} = 1 + 3 = 4 \Omega, \quad \tau = \frac{L}{R_{th}} = \frac{1/4}{4} = \frac{1}{16}
\]

\[
i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{t/\tau}
\]

\[
i(t) = 5\left(1 + e^{-16t}\right) A
\]

\[
v_o(t) = 3i + L \frac{di}{dt} = 15\left(1 + e^{-16t}\right) + \frac{1}{4} (-16)(5)e^{-16t}
\]

\[
v_o(t) = 15 - 5e^{-4t} V
\]
Chapter 7, Solution 59.

Let $i(t)$ be the current through the inductor.
For $t < 0$, $v_s = 0$, $i(0) = 0$

For $t > 0$, $R_{eq} = 4 + (6 \parallel 3) = 6$ Ω and $\tau = \frac{L}{R_{eq}} = \frac{1.5}{6} = 0.25$ sec.

At $t = \infty$, the inductor becomes a short and the current delivered by the 18 volts source is $I_s = 18/[6+(3\parallel 4)] = 18/7.714 = 2.333$ amps. The voltage across the 4-ohm resistor is equal to $18-6(2.333) = 18-14 = 4$ volts. Therefore the current through the inductor is equal to $i(\infty) = 4/4 = 1$ amp.

$$i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau}$$

$$i(t) = 1(1-e^{-4t}) \text{ amps.}$$

$$v_o(t) = L \frac{di}{dt} = (1.5)(1)(-4)(-e^{-4t})$$

$$v_o(t) = [6e^{-4t}]u(t) \text{ volts.}$$
Chapter 7, Solution 60.

Let I be the inductor current.

For $t < 0$, \( u(t) = 0 \rightarrow i(0) = 0 \)

For $t > 0$, \( R_{eq} = 5 \parallel 20 = 4 \, \Omega \), \( \tau = \frac{L}{R_{eq}} = \frac{8}{4} = 2 \)

\[
\begin{align*}
    i(\infty) &= 4 \\
    i(t) &= i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau} \\
    i(t) &= 4 \left( 1 - e^{-t/\tau} \right)
\end{align*}
\]

\[
\begin{align*}
    v(t) &= L \frac{di}{dt} = (8)(-4) \left( -\frac{1}{2} \right) e^{-t/\tau} \\
    v(t) &= 16 e^{-0.5t} \, V
\end{align*}
\]
Chapter 7, Solution 61.

The current source is transformed as shown below.

\[
\begin{align*}
20u(-t) + 40u(t) &+ 0.5 H \\
\tau &= \frac{L}{R} = \frac{1/2}{4} = \frac{1}{8}, \quad i(0) = 5, \quad i(\infty) = 10 \\
i(t) &= i(\infty) + \left[i(0) - i(\infty)\right] e^{t/\tau} \\
i(t) &= (10 - 5e^{-8t})u(t) \text{ A} \\
v(t) &= L \frac{di}{dt} = \left(\frac{1}{2}\right)(-5)(-8)e^{-8t} \\
v(t) &= 20e^{-8t}u(t) \text{ V}
\end{align*}
\]
Chapter 7, Solution 62.

\[ \tau = \frac{L}{R_{eq}} = \frac{2}{3 \parallel 6} = 1 \]

For 0 < t < 1, \( u(t-1) = 0 \) so that
\[ i(0) = 0, \quad i(\infty) = \frac{1}{6} \]
\[ i(t) = \frac{1}{6} (1 - e^{-t}) \]

For t > 1,
\[ i(1) = \frac{1}{6} \left( 1 - e^{-1} \right) = 0.1054 \]
\[ i(\infty) = \frac{1}{3} + \frac{1}{6} = \frac{1}{2} \]
\[ i(t) = 0.5 + (0.1054 - 0.5) e^{-(t-1)} \]
\[ i(t) = 0.5 - 0.3946 e^{-(t-1)} \]

Thus,
\[ i(t) = \begin{cases} \frac{1}{6} (1 - e^{-t}) A & \text{for } 0 < t < 1 \\ 0.5 - 0.3946 e^{-(t-1)} A & \text{for } t > 1 \end{cases} \]
Chapter 7, Solution 63.

For $t < 0$, \( u(-t) = 1 \), \( i(0) = \frac{10}{5} = 2 \)

For $t > 0$, \( u(-t) = 0 \), \( i(\infty) = 0 \)

\[
R_{th} = 5 \| 20 = 4 \, \Omega, \quad \tau = \frac{L}{R_{th}} = \frac{0.5}{4} = \frac{1}{8}
\]

\[
i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau}
\]

\[
i(t) = 2e^{-8t}u(t) \, A
\]

\[
v(t) = L \frac{di}{dt} = \left( \frac{1}{2} \right) (-8)(2)e^{-8t}
\]

\[
v(t) = -8e^{-8t}u(t) \, V
\]

\[2e^{-8t}u(t) \, A, -8e^{-8t}u(t) \, V\]
Chapter 7, Solution 64

Determine the value of $i_L(t)$ and the total energy dissipated by the circuit from $t = 0$ sec to $t = \infty$ sec. The value of $v_{in}(t)$ is equal to $[40-40u(t)]$ volts.

\[\begin{align*}
\text{Solution} \\
\text{Step 1.} & \quad \text{Determine the Thevenin equivalent circuit to the left of the inductor. This} \\
& \text{means we need to find } v_{oc}(t) \text{ and } i_{sc}(t) \text{ which gives us } v_{Thev}(t) = v_{oc}(t) \text{ and } R_{eq} = v_{oc}(t)/i_{sc}(t) \text{ (note, this only works for resistor networks in the time domain). This leads to} \\
& \text{the second circuit shown above.}
\end{align*}\]

Now, with this circuit, we can use the generalized solution to a first order differential equation, $i_L(t) = Ae^{-(t-t_0)/\tau}+B$ where, $t_0 = 0$, $\tau = L/R$, $A+B = i_L(0)$ and $0+B = i_L(\infty)$.

Finally, we can use $w = (1/2)Li_L(t)^2$ to calculate the energy dissipated by the circuit ($w = [(1/2)Li_L(\infty)^2-(1/2)Li_L(0)^2]$).

\[\begin{align*}
\text{Step 2.} & \quad \text{We now determine the Thevenin equivalent circuit. First we need to pick} \\
& \text{a reference node and mark the unknown voltages, as seen above. With the inductor out} \\
& \text{of the circuit, the node equation is simply } [(v_1-v_{in}(t))/40] + [(v_1-0)/40] + 0 \text{ (since} \\
& \text{the inductor is out of the circuit, there is an open circuit where it was) } = 0. \text{This leads to} \\
& [(1/40)+(1/40)]v_1 = (1/40)v_{in}(t) \text{ or } 2v_1 = v_{in}(t) \text{ or } v_1 = 0.5v_{in}(t) = [20–20u(t)] v_{oc}(t) = v_{Thev}(t). \text{Now to short the open circuit which produces} \\
& v_1 = 0 \text{ and } i_{sc} = \frac{1}{2} \left[(0–v_{in}(t))/40\right] = v_{in}(t)/40 = 0.025v_{in}(t) \text{ A.}
\end{align*}\]

\[\begin{align*}
\text{Step 3.} & \quad \text{Now, everything comes together, } R_{eq} = v_{oc}(t)/i_{sc}(t) = 0.5v_{in}(t)/[0.025v_{in}(t)] \\
& = 0.5/0.025 = 20 \Omega. \text{ Next we find } \tau = L/R_{eq} = 10/20 = (1/2) \text{ sec. At } t = 0^–, v_{in}(0^–) = [10–0] V \text{ (note } u(t) = 0 \text{ until } t = 0). \text{ Since it has been at this value for a very long time, the} \\
& \text{inductor can be considered a short and the value of the current is equal to } 20/20 \text{ or } i_L(0^–) = 1 \text{ amp. Since you cannot change the current instantaneously, } i_L(0) = 1 \text{ amp} = A+B. \text{Since} \\
& v_{Thev}(t) = 20–20 = 0 \text{ for all } t > 0, \text{ all the energy in the inductor will be dissipated by} \\
& \text{the circuit and } i_L(\infty) = 0 = B \text{ which means that } A = 1 \text{ and } i_L(t) = [e^{-2t}] u(t) \text{ amps. The} \\
& \text{total energy dissipated from } t = 0 \text{ to } \infty \text{ sec is equal to } [(1/2)Li_L(0^–)^2–(1/2)Li_L(\infty)^2] = \\
& (0.5)10(1)^2–0 = 5 J.
\end{align*}\]
Chapter 7, Solution 65.

Since $v_s = 10[u(t) - u(t - 1)]$, this is the same as saying that a 10 V source is turned on at $t = 0$ and a -10 V source is turned on later at $t = 1$. This is shown in the figure below.

![Graph of voltage vs time](image)

For $0 < t < 1$, $i(0) = 0$, $i(\infty) = \frac{10}{5} = 2$

$$R_{th} = 5 \parallel 20 = 4$$

$$\tau = \frac{L}{R_{th}} = \frac{2}{4} = \frac{1}{2}$$

$$i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{t/\tau}$$

$$i(t) = 2 \left( 1 - e^{-2t} \right) A$$

$$i(1) = 2 \left( 1 - e^{-2} \right) = 1.729$$

For $t > 1$, $i(\infty) = 0$ since $v_s = 0$

$$i(t) = i(1) e^{-(t-1)/\tau}$$

$$i(t) = 1.729 e^{-2(t-1)} A$$

Thus,

$$i(t) = \begin{cases} 
2 \left( 1 - e^{-2t} \right) A & 0 < t < 1 \\
1.729 e^{-2(t-1)} A & t > 1 
\end{cases}$$
Chapter 7, Solution 66.

Using Fig. 7.131, design a problem to help other students to better understand first-order op amp circuits.

Although there are many ways to work this problem, this is an example based on the same kind of problem asked in the third edition.

Problem

For the op-amp circuit of Fig. 7.131, find $v_o$. Assume that $v_s$ changes abruptly from 0 to 1 V at $t=0$. Find $v_o$.

\[ \text{Figure 7.131 For Prob. 7.66.} \]

Solution

For $t<0$, $v_s=0$ so that $v_o(0)=0$

Let $v$ be the capacitor voltage

For $t>0$, $v_s=1$. At steady state, the capacitor acts like an open circuit so that we have an inverting amplifier

\[
v_o(\infty) = -(50k/20k)(1V) = -2.5 \text{ V}
\]

\[
\tau = RC = 50 \times 10^3 \times 0.5 \times 10^{-6} = 25 \text{ ms}
\]

\[
v_o(t) = v_o(\infty) + (v_o(0) - v_o(\infty))e^{-t/\tau} = 2.5(e^{-40t} - 1) \text{ V}
\]
Chapter 7, Solution 67.

The op amp is a voltage follower so that $v_o = v$ as shown below.

![Op amp diagram]

At node 1,

$$\frac{v_o - v_1}{R} = \frac{v_1 - 0}{R} + \frac{v_1 - v_o}{R} \quad \rightarrow \quad v_1 = \frac{2}{3}v_o$$

At the noninverting terminal,

$$C \frac{dv_o}{dt} + \frac{v_o - v_1}{R} = 0$$

$$-RC \frac{dv_o}{dt} = v_o - v_1 = v_o - \frac{2}{3}v_o = \frac{1}{3}v_o$$

$$\frac{dv_o}{dt} = -\frac{v_o}{3RC}$$

$$v_o(t) = V_T e^{-t/3RC}$$

$$V_T = v_o(0) = 5 \text{ V}, \quad \tau = 3RC = (3)(10 \times 10^3)(1 \times 10^{-6}) = \frac{3}{100}$$

$$v_o(t) = 5e^{-100t/3} u(t) \text{ V}$$
Chapter 7, Solution 68.

This is a very interesting problem which has both an ideal solution as well as a realistic solution. Let us look at the ideal solution first. Just before the switch closes, the value of the voltage across the capacitor is zero which means that the voltage at both terminals input of the op amp are each zero. As soon as the switch closes, the output tries to go to a voltage such that both inputs to the op amp go to 4 volts. The ideal op amp puts out whatever current is necessary to reach this condition. An infinite (impulse) current is necessary if the voltage across the capacitor is to go to 8 volts in zero time (8 volts across the capacitor will result in 4 volts appearing at the negative terminal of the op amp). So \( v_o \) will be equal to 8 volts for all \( t > 0 \).

What happens in a real circuit? Essentially, the output of the amplifier portion of the op amp goes to whatever its maximum value can be. Then this maximum voltage appears across the output resistance of the op amp and the capacitor that is in series with it. This results in an exponential rise in the capacitor voltage to the steady-state value of 8 volts.

\[
v_C(t) = V_{\text{op amp max}} (1 - e^{-t/(R_{\text{out}}C)}) \text{ volts, for all values of } v_C \text{ less than 8 V,}
\]

\[
= 8 \text{ V when } t \text{ is large enough so that the 8 V is reached.}
\]
Let $v_x$ be the capacitor voltage.

For $t < 0$, $v_x(0) = 0$

For $t > 0$, the 20 kΩ and 100 kΩ resistors are in series and together, they are in parallel with the capacitor since no current enters the op amp terminals.

As $t \to \infty$, the capacitor acts like an open circuit so that

$$v_o(\infty) = \frac{-4}{10} (20 + 100) = -48$$

$$R_{th} = 20 + 100 = 120 \, \text{kΩ}, \quad \tau = R_{th}C = (120 \times 10^3)(25 \times 10^{-3}) = 3000$$

$$v_o(t) = v_o(\infty) + [v_o(0) - v_o(\infty)] e^{-t/\tau}$$

$$v_o(t) = -48 \left(1 - e^{-t/3000}\right) V = 48(e^{-t/3000} - 1)u(t)V$$
Chapter 7, Solution 70.

Let \( v = \) capacitor voltage.

For \( t < 0 \), the switch is open and \( v(0) = 0 \).

For \( t > 0 \), the switch is closed and the circuit becomes as shown below.

\[
\begin{align*}
\frac{0 - v_s}{R} &= C \frac{dv}{dt} \\
\text{where } v &= v_s - v_o \quad \longrightarrow \quad v_o = v_s - v
\end{align*}
\]

From (1),
\[
\frac{dv}{dt} = \frac{v_s}{RC} = 0
\]
\[
v = -\frac{1}{RC} \int v_s \, dt + v(0) = -\frac{t v_s}{RC}
\]

Since \( v \) is constant,
\[
RC = (20 \times 10^3)(5 \times 10^{-6}) = 0.1
\]
\[
v = \frac{-20t}{0.1} \text{ mV} = -200t \text{ mV}
\]

From (3),
\[
v_o = v_s - v = 20 + 200t
\]
\[
v_o = 20(1 + 10t) \text{ mV}
\]
Chapter 7, Solution 71.

We temporarily remove the capacitor and find the Thevenin equivalent at its terminals. To find $R_{Th}$, we consider the circuit below.

Since we are assuming an ideal op amp, $R_o = 0$ and $R_{Th} = 20 \, \Omega$. The op amp circuit is a noninverting amplifier. Hence,

\[
V_{th} = (1 + \frac{10}{10})V_s = 2V_s = 6V
\]

The Thevenin equivalent is shown below.

Thus,

\[
v(t) = 6(1 - e^{-t/\tau}), t > 0
\]

where $\tau = \frac{R_{th}C}{20 \times 10^{-3} \times 10 \times 10^{-6}} = 0.2$

\[
v(t) = 6(1 - e^{-5t}), t > 0 \, V
\]
Chapter 7, Solution 72.

The op amp acts as an emitter follower so that the Thevenin equivalent circuit is shown below.

Hence,

\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]

\[ v(0) = -2 \text{ V}, \quad v(\infty) = 3 \text{ V}, \quad \tau = RC = (10 \times 10^3)(10 \times 10^{-6}) = 0.1 \]

\[ v(t) = 3 + (-2 - 3)e^{-10t} = 3 - 5e^{-10t} \]

\[ i_o = C \frac{dv}{dt} = (10 \times 10^{-6})(-5)(-10)e^{-10t} \]

\[ i_o = 0.5e^{-10t} \text{ mA,} \quad t > 0 \]
Consider the circuit below.

At node 2,
\[ \frac{v_1 - v_2}{R_1} = C \frac{dv}{dt} \]  \hspace{1cm} (1)

At node 3,
\[ C \frac{dv}{dt} = \frac{v_3 - v_o}{R_f} \]  \hspace{1cm} (2)

But \( v_3 = 0 \) and \( v = v_2 - v_3 = v_2 \). Hence, (1) becomes
\[ \frac{v_1 - v}{R_1} = C \frac{dv}{dt} \]
\[ v_1 - v = R_1 C \frac{dv}{dt} \]

or
\[ \frac{dv}{dt} + \frac{v}{R_1 C} = \frac{v_1}{R_1 C} \]

which is similar to Eq. (7.42). Hence,
\[ v(t) = \begin{cases} \v_{T} & t < 0 \\ v_1 + (v_{T} - v_1)e^{\frac{-t}{\tau}} & t > 0 \end{cases} \]

where \( v_{T} = v(0) = 1 \) and \( v_1 = 4 \)
\[ \tau = R_1 C = (10 \times 10^3)(20 \times 10^{-6}) = 0.2 \]

\[ v(t) = \begin{cases} 1 & t < 0 \\ 4 - 3e^{\frac{-t}{0.2}} & t > 0 \end{cases} \]

From (2),
\[ v_o = -R_f C \frac{dv}{dt} = (20 \times 10^3)(20 \times 10^{-6})(15e^{\frac{-t}{0.2}}) \]
\[ v_o = -6e^{\frac{-t}{0.2}}, \quad t > 0 \]
\[ v_o = -6e^{5t} u(t) \text{ V} \]
Chapter 7, Solution 74.

Let \( v = \) capacitor voltage. For \( t < 0, \quad v(0) = 0 \)

For \( t > 0, \quad i_s = 10 \mu A . \)

Since the current through the feedback resistor is \( i_s, \) then

\[ v_o = -i_s \times 10^4 \text{ volts} = -10^{-5} \times 10^4 = -100 \text{ mV}. \]

It is interesting to look at the capacitor voltage.

\[ i_s = C \frac{dv}{dt} + \frac{v}{R} \]

\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]

It is evident that

\[ \tau = RC = (2 \times 10^{-6})(50 \times 10^3) = 0.1 \]

At steady state, the capacitor acts like an open circuit so that \( i_s \) passes through \( R. \)

Hence,

\[ v(\infty) = i_s R = (10 \times 10^{-6})(50 \times 10^3) = 0.5 \text{ V} \]

Then the voltage across the capacitor is,

\[ v(t) = 500(1-e^{-10t}) \text{ mV}. \]
Chapter 7, Solution 75.

Let $v_1 =$ voltage at the noninverting terminal.
Let $v_2 =$ voltage at the inverting terminal.

For $t > 0$, \[ v_1 = v_2 = v_s = 4 \]
\[
\frac{0 - v_s}{R_1} = i_o, \quad R_1 = 20 \text{k}\Omega \\
v_o = -i_o R
\]
\[(1)\]

Also, \[ i_o = \frac{v}{R_2} + C \frac{dv}{dt}, \quad R_2 = 10 \text{k}\Omega, \quad C = 2 \text{ \mu F} \]
\[ i.e. \quad \frac{-v_s}{R_1} = \frac{v}{R_2} + C \frac{dv}{dt} \]
\[(2)\]

This is a step response.
\[ v(t) = v(\infty) + [v(0) - v(\infty)] e^{\frac{-t}{\tau}}, \quad v(0) = 1 \]
where \( \tau = R_2 C = (10 \times 10^3)(2 \times 10^{-6}) = \frac{1}{50} \)

At steady state, the capacitor acts like an open circuit so that $i_o$ passes through $R_2$. Hence, as $t \to \infty$
\[ \frac{-v_s}{R_1} = i_o = \frac{v(\infty)}{R_2} \]
\[ i.e. \quad v(\infty) = -\frac{R_2}{R_1} v_s = \frac{-10}{20} (4) = -2 \]
\[ v(t) = -2 + (1 + 2)e^{\frac{-t}{50}} \]
\[ v(t) = -2 + 3e^{\frac{-t}{50}} \]

But \[ v = v_s - v_o \]
or \[ v_o = v_s - v = 4 + 2 - 3e^{\frac{-t}{50}} \]
\[ v_o = 6 - 3e^{\frac{-t}{50}} u(t)v \]
\[ i_o = \frac{-v_s}{R_1} = \frac{-4}{20k} = -0.2 \text{ mA} \]
or \[ i_o = \frac{v}{R_2} + C \frac{dv}{dt} = -0.2 \text{ mA} \]
Chapter 7, Solution 76.

The schematic is shown below. For the pulse, we use IPWL and enter the corresponding values as attributes as shown. By selecting Analysis/Setup/Transient, we let Print Step = 25 ms and Final Step = 2 s since the width of the input pulse is 1 s. After saving and simulating the circuit, we select Trace/Add and display \(-V(C1:2)\). The plot of V(t) is shown below.
Chapter 7, Solution 77.

The schematic is shown below. We click Marker and insert Mark Voltage Differential at the terminals of the capacitor to display $V$ after simulation. The plot of $V$ is shown below. Note from the plot that $V(0) = 12\, \text{V}$ and $V(\infty) = -24\, \text{V}$ which are correct.
Chapter 7, Solution 78.

(a) When the switch is in position (a), the schematic is shown below. We insert IPROBE to display i. After simulation, we obtain,

\[ i(0) = 7.714 \, \text{A} \]

from the display of IPROBE.

(b) When the switch is in position (b), the schematic is as shown below. For inductor I1, we let IC = 7.714. By clicking Analysis/Setup/Transient, we let Print Step = 25 ms and Final Step = 2 s. After Simulation, we click Trace/Add in the probe menu and display I(L1) as shown below. Note that \( i(\infty) = 12 \, \text{A} \), which is correct.
Chapter 7, Solution 79.

When the switch is in position 1, $i_0(0) = 12/3 = 4\text{A}$. When the switch is in position 2, $i_0(\infty) = -\frac{4}{5+3} = -0.5\text{A}$, \[ R_{Th} = \frac{3+5}{4} = \frac{8}{3}, \quad \tau = \frac{L}{R_{Th}} = \frac{3}{80} \]

\[ i_0(t) = i_0(\infty) + [i_0(0) - i_0(\infty)]e^{-t/\tau} = -0.5 + 4.5e^{-80t/3} u(t)\text{A} \]
Chapter 7, Solution 80.

(a) When the switch is in position A, the 5-ohm and 6-ohm resistors are short-circuited so that

\[ i_1(0) = i_2(0) = v_o(0) = 0 \]

but the current through the 4-H inductor is \( i_L(0) = \frac{30}{10} = 3 \) A.

(b) When the switch is in position B,

\[ R_{Th} = \frac{3}{6} = 2 \Omega, \quad \tau = \frac{L}{R_{Th}} = \frac{4}{2} = 2 \text{ sec} \]

\[ i_L(t) = i_L(\infty) + [i_L(0) - i_L(\infty)]e^{-t/\tau} = 0 + 3e^{-t/2} = 3e^{-t/2} \text{ A} \]

(c) \( i_1(\infty) = \frac{30}{10 + 5} = 2 \text{ A}, \quad i_2(\infty) = -\frac{3}{9}i_L(\infty) = 0 \text{ A} \)

\[ v_o(t) = L \frac{di}{dt} \quad \longrightarrow \quad v_o(\infty) = 0 \text{ V} \]
Chapter 7, Solution 81.

The schematic is shown below. We use VPWL for the pulse and specify the attributes as shown. In the Analysis/Setup/Transient menu, we select Print Step = 25 ms and final Step = 3 S. By inserting a current marker at one terminal of L1, we automatically obtain the plot of i after simulation as shown below.
Chapter 7, Solution 82.

\[ \tau = RC \quad \rightarrow \quad R = \frac{\tau}{C} = \frac{3 \times 10^{-3}}{100 \times 10^{-6}} = 30 \, \Omega \]
Chapter 7, Solution 83.

\[ v(\infty) = 120, \quad v(0) = 0, \quad \tau = RC = 34 \times 10^6 \times 15 \times 10^{-6} = 510 \text{s} \]

\[ v(t) = v(\infty) + [v(0) - v(\infty)]e^{-t/\tau} \quad \rightarrow \quad 85.6 = 120(1 - e^{-t/510}) \]

Solving for \( t \) gives

\[ t = 510 \ln 3.488 = 637.16 \text{s} \]

speed = \( \frac{4000 \text{m}}{637.16 \text{s}} = 6.278 \text{m/s} \)
Chapter 7, Solution 84.

Let $I_o$ be the final value of the current. Then

$$i(t) = I_o (1 - e^{-t/\tau}), \quad \tau = R/L = 0.16/8 = 1/50$$

$$0.6I_o = I_o (1 - e^{-50t}) \quad \longrightarrow \quad t = \frac{1}{50} \ln \frac{1}{0.4} = 18.33 \text{ ms}.$$
Chapter 7, Solution 85.

(a) The light is on from 75 volts until 30 volts. During that time we essentially have a 120-ohm resistor in parallel with a 6-µF capacitor.

\[
v(0) = 75, \quad v(\infty) = 0, \quad \tau = 120 \times 6 \times 10^{-6} = 0.72 \text{ ms}
\]

\[
v(t_1) = 75 e^{-t_1/\tau} = 30 \quad \text{which leads to } t_1 = -0.72 \ln(0.4) \text{ ms} = 659.7 \mu\text{s of lamp on time.}
\]

(b) \[
\tau = RC = (4 \times 10^6)(6 \times 10^{-6}) = 24 \text{ s}
\]

Since \[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{t/\tau} \]

\[
v(t_1) - v(\infty) = \left[ v(0) - v(\infty) \right] e^{t_1/\tau} \quad (1)
\]

\[
v(t_2) - v(\infty) = \left[ v(0) - v(\infty) \right] e^{t_2/\tau} \quad (2)
\]

Dividing (1) by (2),

\[
\frac{v(t_1) - v(\infty)}{v(t_2) - v(\infty)} = e^{(t_2 - t_1)/\tau}
\]

\[
t_0 = t_2 - t_1 = \tau \ln \left( \frac{v(t_1) - v(\infty)}{v(t_2) - v(\infty)} \right)
\]

\[
t_0 = 24 \ln \left( \frac{75 - 120}{30 - 120} \right) = 24 \ln(2) = 16.636 \text{ s}
\]
Chapter 7, Solution 86.

\[ v(t) = v(\infty) + \left[ v(0) - v(\infty) \right] e^{-t/\tau} \]
\[ v(\infty) = 12, \quad v(0) = 0 \]
\[ v(t) = 12 \left( 1 - e^{-t/\tau} \right) \]
\[ v(t_0) = 8 = 12 \left( 1 - e^{-t_0/\tau} \right) \]
\[ \frac{8}{12} = 1 - e^{-t_0/\tau} \quad \rightarrow \quad e^{-t_0/\tau} = \frac{1}{3} \]
\[ t_0 = \tau \ln(3) \]

For \( R = 100 \, \text{k}\Omega \),
\[ \tau = RC = (100 \times 10^3)(2 \times 10^{-6}) = 0.2 \, \text{s} \]
\[ t_0 = 0.2 \ln(3) = 0.2197 \, \text{s} \]

For \( R = 1 \, \text{M}\Omega \),
\[ \tau = RC = (1 \times 10^6)(2 \times 10^{-6}) = 2 \, \text{s} \]
\[ t_0 = 2 \ln(3) = 2.197 \, \text{s} \]

Thus,
\[ 0.2197 \, \text{s} < t_0 < 2.197 \, \text{s} \]
Chapter 7, Solution 87.

Let $i$ be the inductor current.

For $t < 0$, \[ i(0^-) = \frac{120}{100} = 1.2 \text{ A} \]

For $t > 0$, we have an RL circuit

\[ \tau = \frac{L}{R} = \frac{50}{100 + 400} = 0.1, \quad i(\infty) = 0 \]

\[ i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau} \]

\[ i(t) = 1.2 e^{-10t} \]

At $t = 100 \text{ ms} = 0.1 \text{ s}$,

\[ i(0.1) = 1.2 e^{-1} = 441 \text{ mA} \]

which is the same as the current through the resistor.
(a) \( \tau = RC = (300 \times 10^3)(200 \times 10^{-12}) = 60 \mu s \)
As a differentiator,
\( T > 10\tau = 600 \mu s = 0.6 \text{ ms} \)
i.e. \( T_{\text{min}} = 0.6 \text{ ms} \)

(b) \( \tau = RC = 60 \mu s \)
As an integrator,
\( T < 0.1\tau = 6 \mu s \)
i.e. \( T_{\text{max}} = 6 \mu s \)
Chapter 7, Solution 89.

Since $\tau < 0.1T = 1 \mu s$

\[
\frac{L}{R} < 1 \mu s
\]

\[
L < R \times 10^{-6} = (200 \times 10^3)(1 \times 10^{-6})
\]

\[L < 200 \text{ mH}\]
Chapter 7, Solution 90.

We determine the Thevenin equivalent circuit for the capacitor $C_s$.

$$v_{th} = \frac{R_s}{R_s + R_p} v_i, \quad R_{th} = R_s \parallel R_p$$

The Thevenin equivalent is an RC circuit. Since

$$v_{th} = \frac{1}{10} v_i \quad \rightarrow \quad 1 = \frac{R_s}{R_s + R_p}$$

$$R_s = \frac{1}{9} R_p = \frac{6}{9} = \frac{2}{3} \text{ M}\Omega$$

Also,

$$\tau = R_{th} C_s = 15 \mu s$$

where $R_{th} = R_p \parallel R_s = \frac{6(2/3)}{6 + 2/3} = 0.6 \text{ M}\Omega$

$$C_s = \frac{\tau}{R_{th}} = \frac{15 \times 10^{-6}}{0.6 \times 10^{-6}} = 25 \text{ pF}$$
Chapter 7, Solution 91.

\[ i_0(0) = \frac{12}{50} = 240 \text{ mA} , \quad i(\infty) = 0 \]

\[ i(t) = i(\infty) + \left[ i(0) - i(\infty) \right] e^{-t/\tau} \]

\[ i(t) = 240 e^{-t/\tau} \]

\[ \tau = \frac{L}{R} = \frac{2}{R} \]

\[ i(t_0) = 10 = 240 e^{-t_0/\tau} \]

\[ e^{t_0/\tau} = 24 \quad \longrightarrow \quad t_0 = \tau \ln(24) \]

\[ \tau = \frac{t_0}{\ln(24)} = \frac{5}{\ln(24)} = 1.573 = \frac{2}{R} \]

\[ R = \frac{2}{1.573} = 1.271 \Omega \]
Chapter 7, Solution 92.

\[ i = C \frac{dv}{dt} = 4 \times 10^{-9} \left\{ \begin{array}{ll} \frac{10}{2 \times 10^3} & 0 < t < t_R \\ \frac{-10}{5 \times 10^6} & t_R < t < t_D \end{array} \right. \]

\[ i(t) = \begin{cases} 20 \, \mu A & 0 < t < 2 \, \text{ms} \\ -8 \, \text{mA} & 2 \, \text{ms} < t < 2 \, \text{ms} + 5 \, \mu \text{s} \end{cases} \]

which is sketched below.

(Not to scale)